

Effect of Infill Density and Infill Pattern on the Compressive Strength of Parts Printed by PLA Filament using FDM

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Abstract: *The field of additive manufacturing is growing and discoveries are being made. The 3D printing machines are also being developed to accommodate a wider range of 3D printing materials, including plastics, metals (metal AM powders), composites, filaments, and other materials. There are numerous printing materials available for industrial additive manufacturing. Such materials have their unique characteristics, advantages, and disadvantages. In order to avoid errors in Additive Manufacturing, key elements such as 3D printing material type, texture, cost, printing technique and procedure, and so on must be examined. It can be complex to select the best material for a particular job. PLA (Polylactic acid) is made from sugar cane or cornstarch, both of which are renewable resources. "Black plastic" is another name for it. Because it is safe to use and print, it is frequently used in primary and secondary schools. This is also how FDM screen printing is done. PLA is simple to print because of its low warping impact. It's also possible to print it on a cold surface. When opposed to ABS, it allows for sharper edges and features to be printed. This material comes in a wide range of colours. Polylactic acid (PLA) is the most common material used in fused deposition modelling (FDM). PLA can be used to print a wide range of components including medical implants, household items, and mechanical parts. The mechanical behaviour of the printed item is affected by variations in infill pattern are subjected to compressive tests in the current investigation to examine their behaviour under compressive stresses.*

Keywords: *Fused Deposition Modelling (FDM), Polylactic Acid (PLA), Infill Density, Infill Pattern, Compressive Strength*

I. INTRODUCTION

One of the most significant advantages of 3D printing technology is the ability to produce components with various infill geometries and patterns. Not only does this save material, but it also lowers the overall component cost. Biostructure [1], scaffold constructions [2], micro fabrication [3], light weight UAV (unmanned aerial vehicles) [4], and design of police whistles [5] have all benefited from the 3D printing technique. This method is also employed to investigate the compressive and tensile properties of Natural Sand Stone [6]. Several previous studies have revealed that this approach can be utilized to print a wide range of polymers [7] and composites [8], as well as multi-nozzle extrusion printing [9], [10]. This technique can also print pieces with varying densities [11] and other types of infill generation [12][22]. A review of previous research shows that printing orientation, density, and filler pattern [13], layer thickness and raster angle [14], [15], [16], [3] have a significant impact on mechanical performance of parts such as compressive performance [13], fatigue performance [17], surface roughness tensile strength [18], [19], and maximum flexure properties [20], [21]. This approach can also be connected with design and production data, according

to the research [1]. According to studies, the most important 3D printing parameters are the layer thickness, infill density, and heat treatment [23, 24]. Other studies showed how to optimize the parameters in the Fused Deposition Modeling (FDM) process to increase accuracy and efficiency [25, 26]. The air gap has a significant impact on the wear strength of an FDM-fabricated component [27]. Additionally, the performance of FDM printed parts was examined in relation to other process factors, including building orientation [28, 29] and raster angle [30, [31], [32]. Additionally, it was discovered that the raster angle has less of an impact than print orientation [33].

Additionally, there are a variety of ways whereby processing conditions might affect bonding degree [34]. The mechanical behavior of components created with FDM is also influenced by the raster width and the quantity of contours [35]. In comparison to high density, Baich et al. (2015) showed that low density had cost savings and comparable strength performance for tensile loading [36]. According to Onwubolu et al. (2014), layer and raster thickness should be raised in order to improve the tensile strength of acrylonitrile butadiene styrene (ABS) [37]. In contrast to the other factors, Attaran (2017) asserted that the layer thickness impact on the mechanical properties of ABS material is minimal [38]. Ziemian et al. (2012, 2015) shown experimentally that it is preferable to assign the rasters longitudinally rather than diagonally in order to get the best tensile strength [39, 40].

II. WORK METHODOLOGY

A. Test Specimens

Test specimens were printed using FDM technology. The cross section of the specimen used was 12.7 mm × 12.7 mm with a length of 25.4 mm. The specimens were printed with three different infill patterns i.e. hexagonal, triangular, and linear and three different infill percentages i.e. 20%, 30%, and 40%. The general values for the material properties are following:

TABLE 1. Test Specimen

PROPERTY	VALUE
Bulk Density (g/cm ³)	1.24 g/cm ³
Infill (%)	20% , 30% , 40%
Shell Thickness	0.3 mm
Layer Thickness	0.3 mm
Printing method	FDM
Printer	TEVO-Trantula I3
Printing firm	Tulsiramji Gaikwad- Patil College of Engineering and Technology, Nagpur
Infill Pattern	Hexagonal, linear and triangular
Colour	White
Extruder temperature	220° C
Bed Temperature	80° C

B. Printer Specifications

TABLE 2. Printer Specimen

Name	TEVO-Trantula I3
Number of Extruder	1
Print Technology	Fused Filament Fabrication(FFF)
Build Volume	22.3cm(length) * 22.3 cm (width)* 30.5cm (Height)
Layer Resolution	0.40 mm Nozzle: 200 to 20 Micron
Build Accuracy	±0.2mm
Positioning Accuracy	Z axis 0.0025mm; XY axis 0.011mm
Filament Diameter	1.75mm (±0.02)
Nozzle Diameter	0.4mm
Print Speed	100 mm/s

C. Universal Testing Machine

The Universal Testing Machine used for performing compressive test was model AMT 100 Sold and Serviced by ASI Sales Private Limited Karampura Complex, New Delhi). The specifications of the UTM are:

Max. Capacity 1000 kN

Measuring range - 0 – 1000 kN

Loading unit - Hydraulic Control panel - Electronic Extensometer – Electronic

D. Compressive Test

- Three specimens of each combination were evaluated, with the average value used to draw conclusions. When either plastic deformation or printing layer separation was observed, the specimen was regarded to have failed. The following was the procedure:
- Load the specimen on the UTM
- Start the machine
- Record the load and corresponding deflection
- Plot the curve using excel.

E. Formula used

- Stress = Load applied / cross section area of the specimen
- Strain = Deformation / original length
- Strength to weight ratio = Strength / Mass of specimen
- Young's Modulus = Stress/ Strain

III. RESULTS AND CONCLUSION

1) Compressive strength.

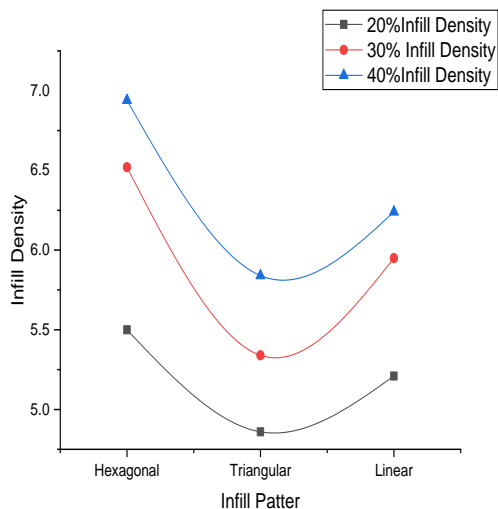
After conducting several experiments the results obtained are gathered in tabular form below: Failure compressive load

TABLE 3. Compressive strength

Infill Pattern	Infill Density		
	20%	30%	40%
Hexagonal	5.5	6.52	6.94
Triangular	4.86	5.34	5.84
Linear	5.21	5.95	6.24

All the values presented above are in Kilo-Newtons.

To visualize the distribution of above data following graph. 1 is plotted:



Graph.1. Relation between Infill density, infill pattern for compressive Strength

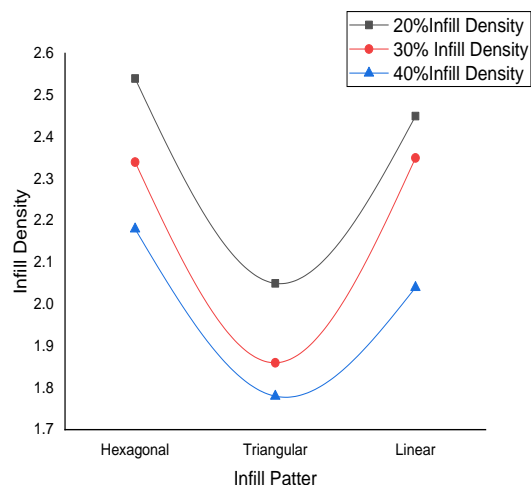
2) Strength to Weight Ratio

Strength to weight ratio is an important consideration when speaking of infill percentages. The following data has been observed in the present experiment:

TABLE 4. Strength to Weight Ratio

Infill Pattern	Infill Density		
	20%	30%	40%
Hexagonal	2.54	2.34	2.18
Triangular	2.05	1.86	1.78
Linear	2.45	2.35	2.04

To visualize above data following graph 2. has been generated:



Graph.2. Relation between Infill density, infill pattern for Strength to Weight Ratio

3) Young’s Modulus

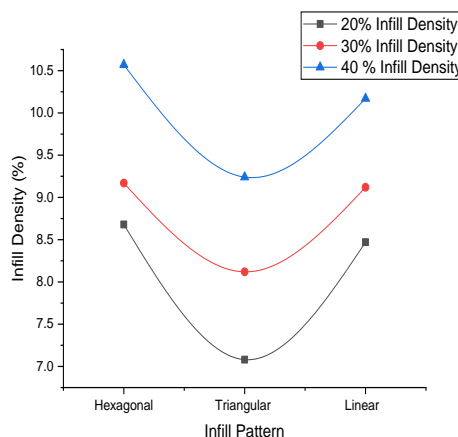
The test data obtained is used to calculate the young’s modulus. The results have been shown below:

TABLE 5. Young’s Modulus

Infill Pattern	Infill Density		
	20%	30%	40%
Hexagonal	8.68	9.17	10.57
Triangular	7.08	8.12	9.24
Linear	8.47	9.12	10.17

All the values presented above are in kN/mm²

When the above data is plotted following graph 3 has been generated.



Graph.3. Relation between Infill density, infill pattern for Young’s Modulus

3) Conclusions

- The maximum yield load was 6.94 kN for a hexagonal design with 40% infill, whereas the minimum yield load was 4.86 kN for a triangular pattern with 20% infill.
- Although the solid specimen yielded at a lower load than the hexagonal with 30%, the load required for further deformation increased after the yield point owing to solid infill, whereas it decreased in all other situations.
- With the exception of solid infill condition, the stress strain study revealed that all infill % and infill patterns combinations display a graph that is quite similar.

- In a hexagonal pattern with 20% infill, the maximum strength to weight ratio was 2.54, while the minimum strength to weight ratio was 1.78 in a specimen with 40% infill.
- The greatest Young's Modulus recorded in the case of a hexagonal pattern with 40% infill was 10.57kN/mm², while the minimum Young's Modulus observed in the case of a triangular infill pattern with 20% infill was 7.08 kN/mm².

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