

Multi-Response Optimization of Wire Electrical Discharge Machining in cutting Nimonic-75

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Abstract:

One such innovative, non-conventional technique is electrical discharge machining of wires. This report describes the findings of an experimental study on Wire Electrical Discharge Machining (WEDM), using Nimonic 75 as a cutting medium. Surface roughness (SR) and material removal rate (MRR) are examples of output responses, while servo voltage, wire feed, pulse on and off times are examples of process variables. Diminishing the harshness and further developing the evacuation pace of the material during machining may prompt better surface qualities and a more noteworthy machining yield. This means that looking into the links between the input and replication parameters is essential. The point of this study is to distinguish the most important info parts involving factual displaying to augment material expulsion rate while diminishing surface harshness. The L29 orthogonal arrays have completed the experimental design with three gradations of each machining parameter. The response surface technique, analysis of variance, and Taguchi method were used to examine the data collected on an optical canvas. The beat on time is the main component in deciding the pace of material evacuation, though the beat of time is the main part in characterizing the surface harshness.

Keywords: *Nimonic, time, voltage, feed, etc.*

I. INTRODUCTION

Modern manufacturing would be impossible without machining techniques. Products are becoming more challenging to produce using conventional machining methods due to the impact of advanced raw material machines. Thus, conventional machining procedures have

fallen out of favour while traditional machining processes have risen in popularity. Advantages of non-traditional machining techniques include the capacity to cut high-strength materials and carry out intricate cuts on work items with intricate structures.

In order to generate complicated cuts in metals that are difficult to mill without resorting to costly grinding or sophisticated forming equipment, the wire electrical discharge machining (WEDM) innovation has become one of the most well-known non-customary creation methods. It is cleverly designed to serve as an alternative to the standard EDM procedure. while cutting. Since the wire doesn't touch the workpiece, it doesn't subject it to the mechanical stress and cutting pressure like milling cutters and grinding wheels do. Metal removal relies on a complex combination of thermal and chemical events; this investigation into its effects on machined parts is an effort to better understand those phenomena.

Despite the fact that the fundamental rule has not changed, WEDM has seen widespread use due to the fact that it can be fully automated and is flexible in producing complicated geometric patterns in a single configuration. In WEDM, a very fine wire serves as the electrode. The wire feed from the reel is controlled by the machine's motion, and it employs electric sparks to logically dissolve an electrically conductive work item as it travels down the track. Copper wire with a zinc coating is used for WEDM, and the wire's diameter is between 0.05 and 0.25 mm. When the voltage is just correct, a spark will bounce off the hole and melt some of the working material. De-ionized water surrounds the wire. Electric sparks are released by the de-ionized water, and any small particles in the hole are flushed out. WEDM is accurate and no burrs are created. The SS317 investigation headed by Chandrasekhar et al. [1] applied a WEDM device. Material abstraction rate and surface roughness were considered to be the basis for how reactions at the output would be categorised. Visual examination showed that when ideal parameters were employed, MRR and SR rose dramatically. The single most important element impacting all replications, it was found, was pulse on time. The E31 steel work that Dhruv H. Gajjar et al. [2] did with molybdenum on WEDM. In this study, we used grey cognition analysis to find the optimal values for MRR, SR, and Kerf width. It was visually seen that an increase in pulse frequency produces a crater that is both larger and more distinctive, leading to a greater amount of surface annoyance. Multi-objective optimisation using WEDM on Inconel 718 was clarified by Mohapatra et al. [3]. By adjusting machining boundaries such wire strain, beat on

time, and heartbeat off time, concrete was created. Visual assessment uncovered that the main component that essentially impacted the results as far as MRR and Kerf Width was beat on time. Mandeep et al. [4] processed Inconel X750 at a higher material reflection rate by utilizing the Taguchi Technique. To research the impact of huge machining boundaries on the extraction rate, investigation of change was utilized. A visual evaluation proposes that the flash hole voltage, top current, on-time, and off-time are fairly significant.

Material abstraction rate, wire wear ratio, and SR were examined by Amitesh et al. [5]. A Nimonic80A work piece was machined using an experimental Taguchi design. Utilising scanning electron microscopy, the machined tests' microstructure is examined. It was observed that the discharge energy caused the work piece's exterior to have deeper, astronomically large holes. Vivek et al. [6] came at the conclusion of their research on inconel 718 material by using replication surface methods. The cathode consisted of zinc-coated brass wire. Out of all the process factors, the pulse on time was shown to be the most important one. Priyaranjansharma et al. [7] conducted a study using inconel 706, a late-developing alloy with aerospace potential. The use of ANOVA has simplified MRR and SR. The beat on time on time and the beat off time appear to greaterly affect the executed elements than miniature construction investigation, metallurgical changes, and miniature hardness assessments of the machine surface. Azam et al. [8] found that changing the machining settings could change the qualities of the activity. Concentrates on the impacts of WEDM cutting boundaries on MRR in titanium amalgam uncovered that MRR expanded with expansions in servo voltage and heartbeat term. It is outwardly obvious that the impact of heartbeat length on release current causes an expansion in MRR. Karim et al. [9] updated the machining attributes of heartbeat on time, beat off time, flushing strain, and wire pressure into particular classes utilizing dark social investigation. The output consistency was found to be most sensitive to the discharge current. The response of various WEDM parameters was studied by Boujelbene et al. [10] when milling high composite steel. Di-ionized dihydrogen monoxide was the collent used in the evaluation of molybdenum wire. It was easily seen that the roughness of the surface grew when the servo voltage was raised. In an effort to reduce surface roughness, Pradeep et al. [11] tried using the Taguchi method to optimise machining settings. To finish the important machining methodology, beat on time, beat off time, and pinnacle current were required. It was shown that more extended beats

expanded surface unpleasantness. The main element was viewed as heartbeat off time, with heartbeat on time trailing behind.

Germain et al. [12] saw that nickel-based compounds are known to be scandalously hard to produce since they hold their mechanical and actual characteristics in any event, when warmed. Due to the low cutting rates, ordinary machining (CM) of these materials is arduous and ineffectual. Kuppan et al. [13] utilized the material evacuation rate (MRR) as their proficiency measure. The reaction surface strategy (RSM) was utilized in the development of the numerical models for this response. The exhibition of inconel 718 was inspected by Prihandana et al. [14] according to the expansion of molybdenum disulfide (MoS₂) powder to the dielectric liquid during miniature EDM. For optimal machining efficiency, Manna and Bhattacharyya assessed and modified the EDM settings in [15]. Gauss elimination was used to create mathematical models. The objective of this demonstrating and improvement study is to come by ideal outcomes for the WEDM interaction. Baburaja et al. investigated the impact of changing input parameters during WEDM milling of aluminium and Hastelloy. [16] using the Taguchi method. Using RSM, Rao K.S. et al.[17] studied how different inputs affected surface roughness in Niobium alloy C-103 during turning. The Taguchi Technique was utilized to improve the machining settings for lead-initiated Ti-6Al-4V amalgam utilizing wire electrical release machining. Numerous studies [18–22] have examined the optimal inconel alloy concentrations. Utilizing an extensive variety of work piece materials, specialists concentrate on WEDM with the utilization of investigations, Taguchi examination, the reaction surface technique, and multi reaction enhancement [23-25]. Mathematical models were developed, and verification experiments were conducted, to ensure that the models were accurate representations of the processes involved in creating the Nimonic -75 specimens that were treated using the WEDM method. Machinable surface roughness and removal rate as a function of process parameter variation are also studied.

2. MATERIALS AND METHODS

Trials were performed using a CNC wire EDM (ULTRACUT -843), as shown in Figure 1. Nimonic-75, a material with dimensions of 70 millimetres by 50 millimetres by 10 millimetres, utilised as the cutting toolwire. As the dielectric, deionized water was kept at a constant temperature of 20 degrees Celsius. Table I displays the material composition of the workpiece

in terms of its chemical make-up.

TABLE I

%C	%si	%Mn	%Cr	%Fe	%Cu	%Ti	%Ni
0.097	0.193	0.295	20.155	3.18	0.055	0.225	75.285

Machining boundaries like servo voltage, beat on time, beat off time, and wire feed rates might be displayed in Table 2. Harshness and expulsion rate toward the final result are displayed in Table 3. Writing audits were utilized to lay out adequate info ranges for the boundaries. A Taly Surf harshness analyzer was utilized to measure the surface's unpleasantness. You might work out the material expulsion rate from the high-accuracy gauging device by utilizing the primary condition underneath. The exploratory arrangement is displayed in Fig. 1.

$$(Initial\ weight-Final\ weight) / (\rho \times time) \text{ -----(1)}$$

$$\rho\text{-Density of material } -8.37\text{gm/cm}^3$$



Fig 1: Experimental setup

TABLE II - Machining parameters

Input parameters	Units	Level 1	Level 2	Level 3
Pulse on time	μs	107	109	111
Pulse off time	μs	60	58	56
Servo voltage	v	15	20	25
Wire feed	m / min	1	2	3

TABLE III- The relationship between machining settings and output quality.

Exp No	Pulson time (μs)	Pulse off time (μs)	Servo voltage (v)	Wire feed m/min	SR (μm)	MRR (mm^3/min)
1	109	58	20	2	1.164	91.677
2	111	56	20	2	1.484	94.639
3	111	58	15	2	1.496	94.651
4	109	58	25	1	1.054	92.569
5	109	56	20	3	1.313	92.773
6	111	58	20	1	1.355	94.543
7	109	56	25	2	1.182	92.665
8	109	58	20	2	1.184	92.677
9	109	60	15	2	1.186	92.688
10	107	58	25	2	0.883	90.703
11	109	60	20	3	1.103	92.580
12	109	58	20	2	1.184	92.677
13	107	58	20	3	1.013	90.811
14	109	58	20	2	1.184	92.677
15	111	58	20	3	1.402	94.443
16	111	60	20	2	1.274	94.446
17	109	58	20	2	1.184	92.677
18	109	58	15	3	1.315	92.885
19	109	60	20	1	1.056	92.580
20	107	58	20	1	0.967	90.811

21	109	56	20	1	1.266	92.773
<i>22</i> <i>Research paper</i>	107	58	15	2	1.097	90.919
23	109	58	15	1	1.268	92.785
24	109	60	25	2	0.972	92.472
25	109	58	25	3	1.100	92.569
26	107	60	20	2	0.885	90.714
27	109	56	15	2	1.297	92.881
28	107	56	20	2	1.095	90.907
29	111	58	25	2	1.171	93.435

III RESULTS AND DISCUSSION

III.I EFFECTS OF SURFACE ROUGHNESS

As on and off times grow, the experimental data shows that surface irregularity continues to diminish. However, once the duration is 5s and the Discharge current is 2000A, the roughness of the material is minimal. Figure 2 is a graphical representation of a comparison between the predicted values of SR square from the mathematical model and the experimental data. It has been determined via research that the pulse on/off time contributes the most to SR, whereas the discharge current and servo speed contribute the least. The ideal surface roughness is shown in Fig. 3 as A3, B1, C1, and D3.

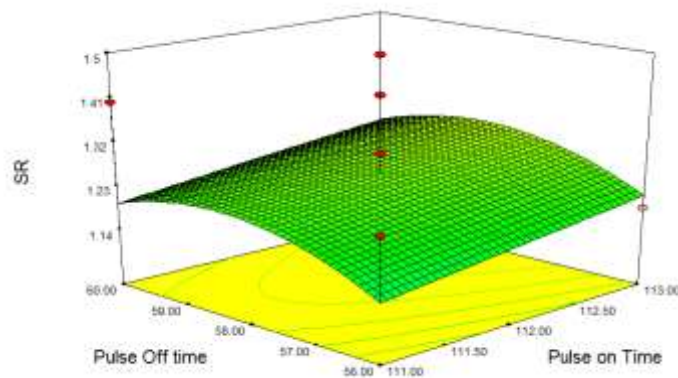


Fig 2: SR Roughness of the Surface rhythmic on/off pulsing

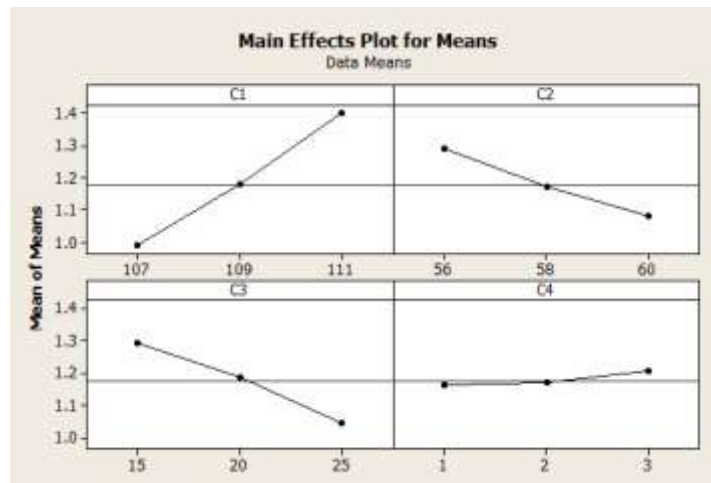


Fig 3: Optimal level of surface roughness

III.II ASSESSING THE IMPACT OF KEY PROCESS FACTORS ON MRR

The Table.III explanation shows that MRR tends to extend to increasing levels of on-time and speedy rates, which climax in high rates of wire EDM, which culminate inside high rates of material. Fig. 4 is a graphical representation of the comparison between the mathematical model's anticipated values of MRR and the experimental values. Pulse on and servo speed have been shown to have the greatest impact on maximum material removal efficiency (MRR), whereas discharge current and off-time have been found to have the least. Two quality goals, material abstraction rate and surface irregularity, were eliminated after the trimming. After doing an analysis of knowledge, a review of the model is crucial. Fig. 5 shows the optimal removal rate as A3.B1.C1.D1.

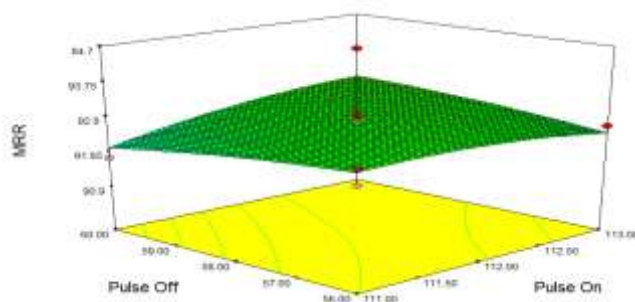


Fig 4: The relationship between the MRR surface response and the on/off interval

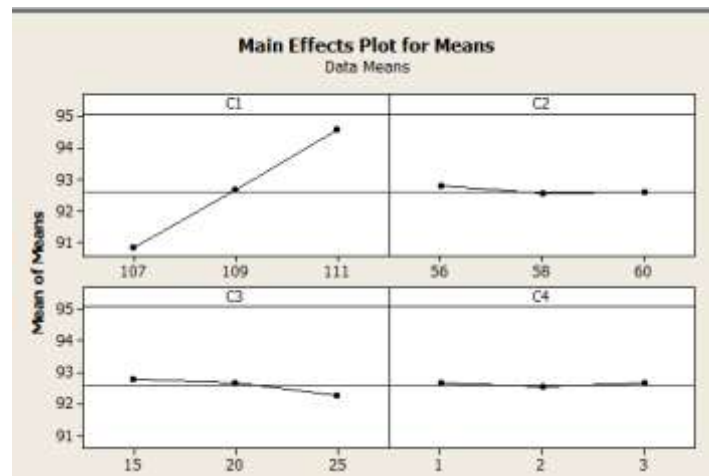


Fig 5: Maximum effective rate of material removal

III.III ANALYSIS OF VARIANCE AND RSM

When we perform an ANOVA on the models in the aforementioned tables, we discover that all of them have P-values less than 0.05, suggesting that they are statistically significant and that the model's terms have the most impact on the replications at the 97.4% level of confidence. In the end, you just need equations 2 and 3 to reproduce a wide range of performance measurements like SR and MRR. The surface unpleasantness, relapse measurements, and pace of material evacuation differences are displayed in Tables IV, V, and VI, in a specific order.

$$SR = 1.09 + 0.086 * A - 0.045 * B - 0.050 * C + 0.011 * D + 4.047E-003 * A * B - 8.209E-003 * A * C - 8.891E-004 * A * D - 0.013 * B * C + 4.753E-004 * B * D + 4.848E-004 * C * D - 4.436E-003 * A^2 - 2.041E-003 * B^2 - 7.230E-003 * C^2 + 4.402E-003 * D^2 \text{-----(2)}$$

$$MRR = 92.73 + 0.14 * A - 0.06 * B + 0.12 * C + 0.028 * D + 0.30 * A * B + 0.45 * A * C - 0.21 * A * D + 0.86 * B * C + 0.91 * B * D - 0.93 * C * D - 0.17 * A^2 - 0.083 * B^2 + 0.30 * C^2 - 0.36 * D^2 \text{-----(3)}$$

Table 4. Surface Roughness and the ANOVA Test

Source	Sum of Squares	df	Mean Square	F Value	P value Prob > F	
Model	0.146697779	14	0.010478413	76.73251308	< 0.0001	significant
A-A	0.089347672	1	0.089347672	654.285297	< 0.0001	
B-B	0.024250364	1	0.024250364	177.5833235	< 0.0001	
C-C	0.030027083	1	0.030027083	219.8857426	< 0.0001	
D-D	0.001378379	1	0.001378379	10.09374928	0.0067	
AB	6.55121E-05	1	6.55121E-05	0.479739676	0.4999	
AC	0.000269547	1	0.000269547	1.973868773	0.1818	
AD	3.16189E-06	1	3.16189E-06	0.023154216	0.8812	
BC	0.000673899	1	0.000673899	4.934905283	0.0433	
BD	9.03616E-07	1	9.03616E-07	0.006617101	0.9363	
CD	9.39939E-07	1	9.39939E-07	0.00688309	0.9351	
A ²	0.000127649	1	0.000127649	0.934759971	0.3500	
B ²	2.7031E-05	1	2.7031E-05	0.197945949	0.6632	
C ²	0.000339051	1	0.000339051	2.482842613	0.1374	
D ²	0.00012567	1	0.00012567	0.920269984	0.3537	
Residual	0.001911807	14	0.000136558			
Lack of Fit	0.001843685	10	0.000184369	10.82573778	0.0173	significant
Pure Error	6.81223E-05	4	1.70306E-05			
Cor Total	0.148609586	28				

TABLE V Regression Statistics

Regression Statistics	
Multiple R	0.987
R Square	0.974
Adjusted R Square	0.970
Standard Error	0.026974
Observations	29

TABLE VI. Analysis of Variance for Material Clearance

Source	Sum of Squares	df	Mean Square	F Value	p-value Prob > F	
Model	13.47198371	14	0.962284551	0.506880418	0.8920	not significant
A-A	0.234081333	1	0.234081333	0.12330162	0.7307	
B-B	0.051221333	1	0.051221333	0.026980679	0.8719	
C-C	0.177940066	1	0.177940066	0.093729381	0.7640	
D-D	0.009478692	1	0.009478692	0.004992872	0.9447	
AB	0.369664	1	0.369664	0.194719371	0.6658	
AC	0.802618892	1	0.802618892	0.422777025	0.5261	
AD	0.182645117	1	0.182645117	0.096207752	0.7610	
BC	2.950252817	1	2.950252817	1.554036568	0.2330	
BD	3.303778817	1	3.303778817	1.740255297	0.2083	
CD	3.460976537	1	3.460976537	1.823058711	0.1984	
A ²	0.187671606	1	0.187671606	0.098855439	0.7578	
B ²	0.044450086	1	0.044450086	0.023413946	0.8806	
C ²	0.587921685	1	0.587921685	0.309685933	0.5867	
D ²	0.818029094	1	0.818029094	0.430894301	0.5222	
Residual	26.57822878	14	1.898444913			
Lack of Fit	19.55886259	10	1.955886259	1.114565734	0.4992	not significant
Pure Error	7.019366193	4	1.754841548			
Cor Total	40.0502125	28				

IV CONFIRMATION TEST

Confirmation experiments are performed to verify the results of previous experiments. An experiment to corroborate the results was performed in this research, and the best possible

significance level was used for the parameter. Experiments have shown that an SR of 0.756 and an MRR of 94.7476 mm³/min are the best parameters. Table VII displays the verification outcomes.

Table VII

S.No	Parameters	Initial level	Optimal level	Improvement (%)
1	SR	A1-B1-C3-D2 (µm)	A1-B1-C3-D1 (µm)	
		0.777	0.756	2.702
2	MRR	InitialLevel	A3-B1-C3 (mm ³ /min)	
		90.606	94.7476	4.371

V CONCLUSIONS

The review analyzed the effect of a few boundaries, for example, wire victual rate, servo voltage, beat on and beat off times, on a superficial level harshness and material reflection pace of Nimonic-75 during wire electrical release machining (WEDM). It has been shown that info cycle boundaries altogether affect limiting heartbeat on time. In view of examination of change, it is shown that both heartbeat off time and wire victual rate affect surface harshness. The material assimilation rate is fundamentally affected by the beat periods, both on and off. For a smooth surface, the ideal upsides of servo voltage, victual wire rate, beat on-time, and heartbeat off-time are 107, 60, 25, and 1. A heartbeat on season of 111, a heartbeat off season of 56, a servo volt of 15, and a wire victual pace of 3 are the ideal boundaries for the material deliberation rate. Surface unpleasantness changed by 14.57 percent and the material deliberation rate by 4.25 percent, as per the compliance discoveries.

REFERENCES

- [1] Y. Chandra Sekhar Reddy, T. Pratheep Reddy, 2017. Optimization of WEDM process Parameters on SS 317 using Grey relational analysis, International Research Journal of Engineering and Technology, 2395-0072.
- [2] Dhruv H. Gajjar, Jayesh V. Desai, 2015. Optimization of MRR, Surface Roughness and KERF Width in WEDM using Molybdenum wire, An International Journal for Research in Education. 4, 2.
- [3] K.D. Mohapatra, S.K. Sahoo, 2017. A multi objective optimization of gear cutting in WEDM of Inconel 718 using TOPSIS method, DOI:10.5267/j.dsl.2017.6.002.
- [4] Mandeep Kumar, Hari Singh 2016. Optimization of process parameters of WEDM for Material Removal Rate using Taguchi technique”, Indian Journal Engineering and Material Sciences, 23, 223-320.
- [5] Amitesh Goswami, Jatinder Kumar, 2017 . Investigation of surface integrity, material removal rate and wire wear ratio for WEDM of Nimonic 80A alloy using GRA and Taguchi method”, Engineering Science and Technology, an International Journal, 17,4, DOI: [10.1016/j.jestch.2014.05.002](https://doi.org/10.1016/j.jestch.2014.05.002).
- [6] Vivek Aggarwal, Sehijpal Singh Khangura Parametric modelling and optimization for WEDM of Inconel 718 using response surface methodology, Int J Adv. ManufTechnol, DOI 10.1007/s00170-015-6797-8.
- [7] Priyaranjan Sharma, D. Chakradhar, 2017. Analysis and Optimization of WEDM performance characteristics of Inconel 706 for Aerospace applications, Springer, DOI 10.1007/s12633-017-9549-6.
- [8] N. Azam, M. Afendi, 2016, Effect of WEDM cutting parameters on Material Removal Rate of Titanium Alloy, AIP conference proceedings 1756, 060001; doi: 10.1063/1.4958775, 2016.
- [9] Md. Karim Baig, N. Venkaiah, “Parametric optimization of WEDM for Hastelloy C276, using GRA method”, International Journal of Engineering Development of Research,
- [10] M. Boujelbene, S. Ezzdini, 2017. Investigation on the surface roughness of high steel material after WEDM process, International journal of advanced and applied sciences, 4(6), 130-136.

- [11] Pradeep Kumar Karsh, Hari Singh, 2016. Optimization of process parameters for Surface roughness of Inconel 625 in WEDM by using Taguchi method”, IOSR Journal of Mechanical and Civil Engineering and Technology (IRJET), 3,3.
- [12] G. Germain, J.L. Lebrun, T. Braham-Bouchnak, D. Bellett, S. Auger, 2008, Laser assisted machining of Inconel 718 with carbide and ceramic inserts, Int. J. Mater. Form. 523–526.
- [13] P. Kuppan, A. Rajadurai, S. Narayanan, 2008. Influence of EDM process parameters in deep hole drilling of Inconel 718, Int. J. Adv. Manuf. Technol. 38,74–84.
- [14] G.S. Prihandana, T. Sriani, M. Mahardika, M. Hamdi, N. Miki, Y.S. Wong, K. Mitsui, 2014, Application of powder suspended in dielectric fluid for fine finish micro-EDM of Inconel 718, Int. J. Adv. Manuf. Technol. 75 , 599–613.
- [15] A. Manna, B. Bhattacharyya, 2006. Taguchi and Gauss elimination method: A dual Response approach for parametric optimization of CNC wire cut EDM of Al/ SiCMMC, Int. J. Adv. Manuf. Technol. 28, 67–75.